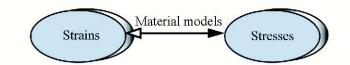
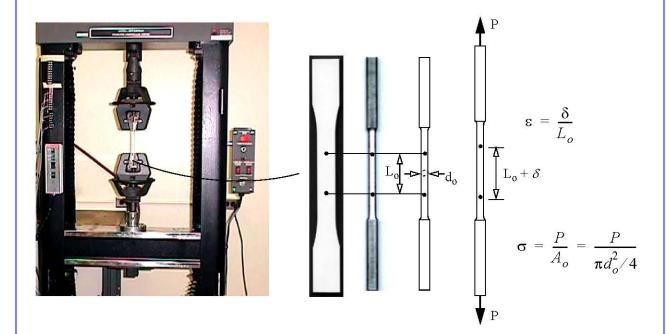
# **Mechanical Properties of Materials**

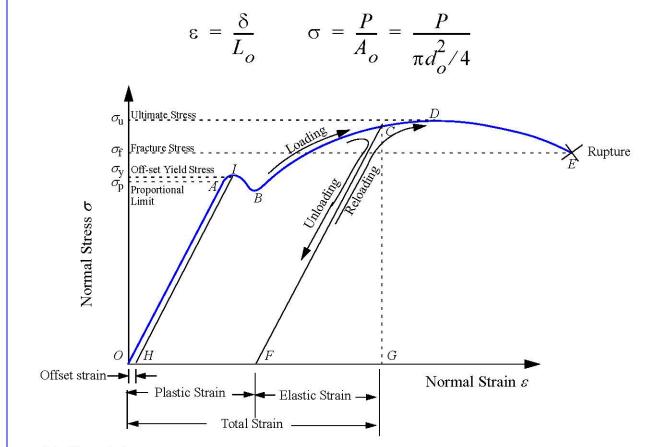


### Learning objectives

- Understand the qualitative and quantitative description of mechanical properties of materials.
- Learn the logic of relating deformation to external forces.

# **Tension Test**





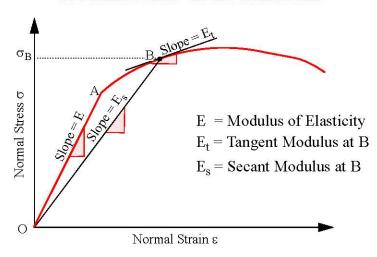
re 3.1 Stress-strain curve.

### **Definitions**

- The point up to which the stress and strain are linearly related is called the proportional limit.
- The largest stress in the stress strain curve is called the ultimate stress.
- The stress at the point of rupture is called the **fracture** or **rupture** stress.
- The region of the stress-strain curve in which the material returns to the undeformed state when applied forces are removed is called the elastic region.
- The region in which the material deforms permanently is called the plastic region.
- The point demarcating the elastic from the plastic region is called the yield point. The stress at yield point is called the yield stress.
- The permanent strain when stresses are zero is called the plastic strain.
- The off-set yield stress is a stress that would produce a plastic strain corresponding to the specified off-set strain.
- A material that can undergo large plastic deformation before fracture is called a ductile material.
- A material that exhibits little or no plastic deformation at failure is called a brittle material.
- Hardness is the resistance to indentation.
- The raising of the yield point with increasing strain is called strain hardening.
- The sudden decrease in the area of cross-section after ultimate stress is called necking.

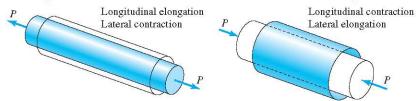


# **Material Constants**



 $\sigma = E\varepsilon$  -----Hooke's Law

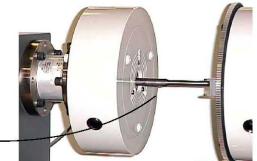
E Young's Modulus or Modulus of Elasticity



• Poisson's ratio:

$$v = -\left(\frac{\varepsilon_{lateral}}{\varepsilon_{longitudnal}}\right)$$

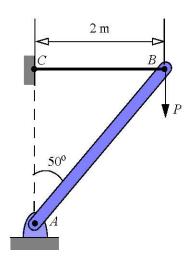


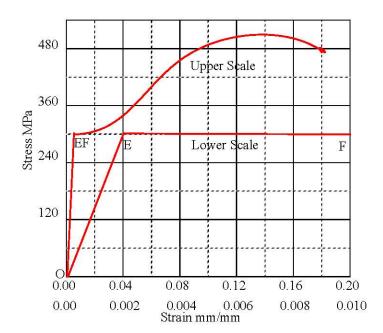


 $\tau = G\gamma$ 

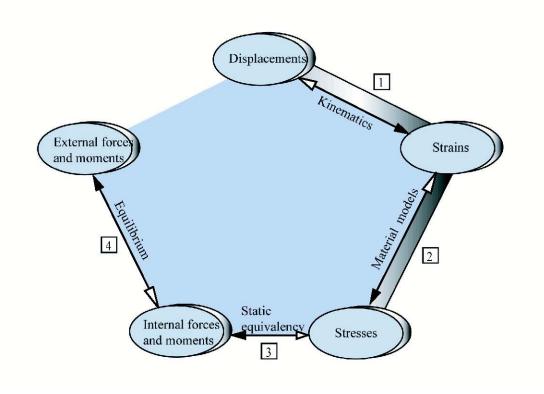
G is called the Shear Modulus of Elasticity or the Modulus of Rigidity

C3.2 A rigid bar AB of negligible weight is supported by cable of diameter 6 mm, as shown. The cable is made from a material that has a stress-strain curve shown. (a) Determine the extension of the cable when P = 10 kN. (b) What is the permanent deformation in BC when the load P is removed?





# Logic in structural analysis



C3.3 A roller slides in a slot by the amount  $\delta_P = 0.25$  mm in the direction of the force F. Both bars have an area of cross-section of  $A = 100 \text{ mm}^2$  and a Modulus of Elasticity E = 200 GPa. Bar AP and BP have lengths of  $L_{AP} = 200 \text{ mm}$  and  $L_{BP} = 250 \text{ mm}$  respectively. Determine the applied force F.

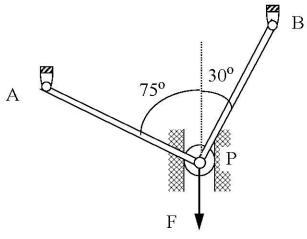


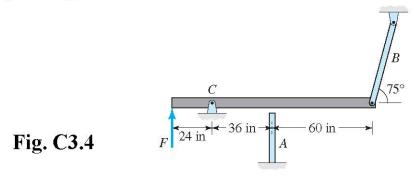
Fig. C3.3

### Failure and factor of safety

• Failure implies that a component or a structure does not perform the function it was designed for.

$$K_{safety} = \frac{Failure\ producing\ value}{Computed(allowable)value}$$
 3.1

C3.4 A gap of 0.004 in. exists between a rigid bar and bar A before a force F is applied (Figure P3.4). The rigid bar is hinged at point C. Due to force F the strain in bar A was found to be  $-500 \,\mu$ in/in. The lengths of bars A and B are 30 in. and 50 in., respectively. Both bars have cross-sectional areas A = 1 in.², a modulus of elasticity E = 30,000 ksi, and yield stress of 35 ksi. Determine (a) the applied force F. (b) the factor of safety if yielding is to be avoided.



**Fig. C3.4** 

### **Isotropy and Homogeneity**

Linear relationship between stress and strain components:

$$\begin{split} & \varepsilon_{xx} \, = \, C_{11} \sigma_{xx} + C_{12} \sigma_{yy} + C_{13} \sigma_{zz} + C_{14} \tau_{yz} + C_{15} \tau_{zx} + C_{16} \tau_{xy} \\ & \varepsilon_{yy} \, = \, C_{21} \sigma_{xx} + C_{22} \sigma_{yy} + C_{23} \sigma_{zz} + C_{24} \tau_{yz} + C_{25} \tau_{zx} + C_{26} \tau_{xy} \\ & \varepsilon_{zz} \, = \, C_{31} \sigma_{xx} + C_{32} \sigma_{yy} + C_{33} \sigma_{zz} + C_{34} \tau_{yz} + C_{35} \tau_{zx} + C_{36} \tau_{xy} \\ & \gamma_{yz} \, = \, C_{41} \sigma_{xx} + C_{42} \sigma_{yy} + C_{43} \sigma_{zz} + C_{44} \tau_{yz} + C_{45} \tau_{zx} + C_{46} \tau_{xy} \\ & \gamma_{zx} \, = \, C_{51} \sigma_{xx} + C_{52} \sigma_{yy} + C_{53} \sigma_{zz} + C_{54} \tau_{yz} + C_{55} \tau_{zx} + C_{56} \tau_{xy} \\ & \gamma_{xy} \, = \, C_{61} \sigma_{xx} + C_{62} \sigma_{yy} + C_{63} \sigma_{zz} + C_{64} \tau_{yz} + C_{65} \tau_{zx} + C_{66} \tau_{xy} \end{split}$$

- An isotropic material has a stress-strain relationships that are independent of the orientation of the coordinate system at a point.
- A material is said to be homogenous if the material properties are the same at all points in the body. Alternatively, if the material constants  $C_{ij}$  are functions of the coordinates x, y, or z, then the material is called non-homogenous.

For Isotropic Materials: 
$$G = \frac{E}{2(1+v)}$$

# Generalized Hooke's Law for Isotropic Materials

• The relationship between stresses and strains in three-dimensions is called the Generalized Hooke's Law.

$$\begin{split} \varepsilon_{xx} &= [\sigma_{xx} - v(\sigma_{yy} + \sigma_{zz})]/E \\ \varepsilon_{yy} &= [\sigma_{yy} - v(\sigma_{zz} + \sigma_{xx})]/E \\ \varepsilon_{zz} &= [\sigma_{zz} - v(\sigma_{xx} + \sigma_{yy})]/E \\ \gamma_{xy} &= \tau_{xy}/G \\ \gamma_{yz} &= \tau_{yz}/G \\ \gamma_{zx} &= \tau_{zx}/G \end{split} \qquad \qquad G = \frac{E}{2(1+v)} \\ \gamma_{zx} &= \tau_{zx}/G \\ \begin{cases} \varepsilon_{xx} \\ \varepsilon_{yy} \\ \varepsilon_{zz} \end{cases} = \frac{1}{E} \begin{bmatrix} 1 & -v & -v \\ -v & 1 & -v \\ -v & -v & 1 \end{bmatrix} \begin{cases} \sigma_{xx} \\ \sigma_{yy} \\ \sigma_{zz} \end{cases} \end{split}$$

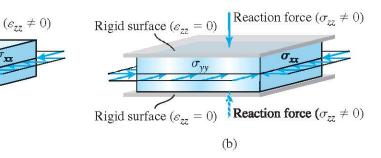
### **Plane Stress and Plane Strain**

Plane Stress 
$$\begin{bmatrix} \sigma_{xx} & \tau_{xy} & 0 \\ \tau_{yx} & \sigma_{yy} & 0 \\ 0 & 0 & 0 \end{bmatrix} \xrightarrow{\text{Generalized Hooke's Law}} \begin{bmatrix} \varepsilon_{xx} & \gamma_{xy} & 0 \\ \gamma_{yx} & \varepsilon_{yy} & 0 \\ 0 & 0 & \varepsilon_{zz} = -\frac{\mathbf{v}}{E}(\sigma_{xx} + \sigma_{yy}) \end{bmatrix}$$
Plane Strain 
$$\begin{bmatrix} \varepsilon_{xx} & \gamma_{xy} & 0 \\ \gamma_{yx} & \varepsilon_{yy} & 0 \\ 0 & 0 & 0 \end{bmatrix} \xrightarrow{\text{Generalized Hooke's Law}} \begin{bmatrix} \sigma_{xx} & \tau_{xy} & 0 \\ \tau_{yx} & \sigma_{yy} & 0 \\ 0 & 0 & \sigma_{zz} = \mathbf{v}(\sigma_{xx} + \sigma_{yy}) \end{bmatrix}$$

#### Plane Stress

# Free surface $(\sigma_{zz}=0)$ $(\varepsilon_{zz}\neq0)$ Free surface $(\sigma_{zz}=0)$ (a)

#### Plane Strain



C3.5 A 2in x 2 in square with a circle inscribed is stressed as shown Fig. C3.5. The plate material has a Modulus of Elasticity of E = 10,000 ksi and a Poisson's ratio v = 0.25. Determine the major and minor axis of the ellipse formed due to deformation assuming (a) plane stress. (b) plane strain.

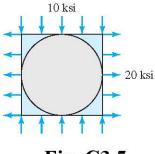


Fig. C3.5

### **Class Problem 3.1**

The stress components at a point are as given. Determine  $\varepsilon_{xx}$  assuming (a) Plane stress (b) Plane strain

$$\sigma_{xx} = 100 \ MPa(T)$$

$$\sigma_{yy} = 200 \ MPa(C)$$

$$\tau_{xy} = -125 \ MPa$$

$$E = 200 \ GPa$$

$$v = 0.25$$

# Common Limitations to Theories in Chapters 4-7

- The length of the member is significantly greater (approximately 10 times) then the greatest dimension in the cross-section.
- We are away from regions of stress concentration, where displacements and stresses can be three-dimensional.
- The variation of external loads or changes in the cross-sectional area is gradual except in regions of stress concentration.
- The external loads are such that the axial, torsion and bending problems can be studied individually.